ROLLWAY T 16050 USA

Thrust

Unmounted bearing assembly consisting of through hardened housing and shaft plate (raceways) with cylindrical or tapered rolling elements separated by a centrifugally cast brass retainer (cage). Thrust bearings are ideal for applications with loads parallel to the shaft.

Bearing Configurations

Single Or Multistage

Rolling Element Styles

Cylindrical Or Tapered

Bore Diameter Size Range

1” To 18” (25.4 mm To 457 mm)

Materials

Bearing Quality Steel

Thrust Selection Guide

	Type	Description	Size Range
	Txxx	Cylindrical Roller Thrust	6” - 34”
	Atxxx	Aligning Cylindrical Roller Thrust	6” - 35”
	T-xxx	Tapered Roller Thrust	8” - 33”
	T-xxxx-F	T-flat Tapered Roller Thrust	10.5” - 34”
	T-xxxx-FS	Aligning T-Flat Tapered Roller Thrust	19” - 34”
	CTxxx	Crane Hook Thrust	3” - 18.5”
	WCTxxx	Crane Hook Thrust w/ Fitting	3” - 18.5”

* For estimating purpose only, individually sizes may vary and are subject to change without notification

Design Characteristics						Features		
Static Load	Dynamic Load	Reversing Load	Higher Speed	Horizontal Installation	Relative Base Cost *	Self Aligning	Grease Fitting	Page No.
◒	◒	○	●	◒	$			F-13
◒	◒	○	●	◒	$$	S		F-17
◒	●	○	◒	●	$$			F-27
◒	●	○	◒	●	$$			F-29
◒	●	○	◒	●	$$	S		F-30
◒	◒	○	○	◒	$$		S	F-21
◒	◒	○	○	◒	$$			F-21

Misalignment Capability

External Greasing

O = Optional
S = Standard
○ = Not Recommended

○ ◒ ◒ ◒ ●

Poor ⟷ Best

Thrust Selection Guide

	Type	Description	Size Range
	TAB-xxxx	2 Stage Tandem Thrust	4.3” - 34”
	TAC-xxxx	3 Stage Tandem Thrust	3.5” - 34”
	TAD/TMD-xxxx	4 Stage Tandem Thrust	3.9” - 12”
	TAF/TMF-xxxx	6 Stage Tandem Thrust	3.5” - 6”
	TMH-xxxx	8 Stage Tandem Thrust	3.5” - 14”

* For estimating purpose only, individually sizes may vary and are subject to change without notification

Design Characteristics						Features			
Static Load	Dynamic Load	Reversing Load	Higher Speed	Horizontal Installation	Relative Base Cost *	Self Aligning	Grease Fitting	Oil Holes / Pathway	Page No.
●	●	○	◒	◒	$$$			S	F-35
●	●	○	◒	◒	$$$			S	F-36
●	●	○	◒	◒	$$$			S	F-37
●	●	○	◒	◒	$$$			S	F-38
●	●	○	◒	◒	$$$			S	F-39

Misalignment Capability

External Greasing

Relubrication and Long Bearing Life

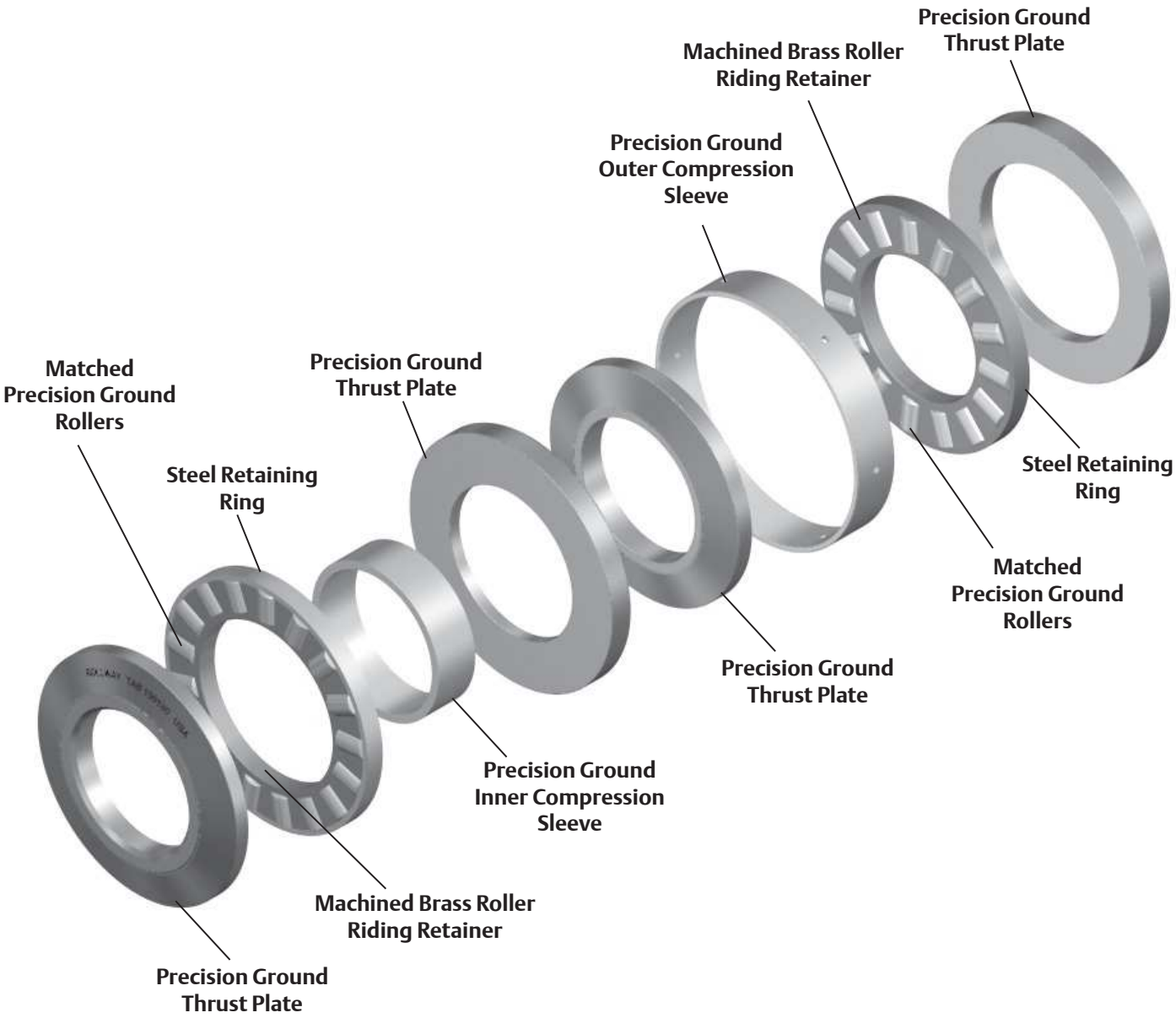
O = Optional
S = Standard
○ = Not Recommended

○ ◔ ◒ ● ●

Poor ⟷ Best

Rollway Tandem Thrust Bearings

Rollway Tandem Thrust bearings are also known as “multi-stage thrust” bearings. Tandem Thrust bearings are comprised of “stages” which include precision ground and matched thrust plates and compression sleeves separated by cylindrical roller assemblies. This design enables the Tandem Thrust bearings to provide a solution in a radial restricted envelope. The bearings are available in multiple stages, 2-8 to accommodate your design requirements. Depending on your preference, these bearings are available in a wide variety of sizes and options as illustrated on the pages to follow.



Features and Benefits

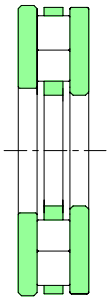
Minimal Backing Support Requirements

The tandem thrust design permits the use of minimal shaft and housing shoulders required by some applications. The cantilevering action of the thrust plates and use of compression sleeves enable these bearings to be used effectively where only minimal shaft and housing shoulder exist.

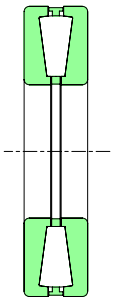
Space Saving Design

The use of a tandem thrust bearing enables the designer to create a gearbox with high thrust capacity within a small space. The end result is a gearbox with a smaller footprint. The drawings below are a comparison of three different thrust bearings with similar dynamic capacity. This illustrates the dramatic reduction in outside diameter associated with the tandem thrust bearings.

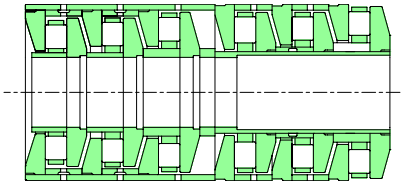
T752 Cylindrical Thrust
Dynamic Capacity=375,500 lbs
O.D.=14”



T-511 Tapered Thrust
Dynamic Capacity=322,500 lbs
O.D.=10.5”



TMF-030127-201
6-Stage Tandem Thrust
Dynamic Capacity=329,900 lbs
O.D.=5”



Features and Benefits continued

Matched Precision Ground Rollers

Rollers are manufactured from Carburized Bearing Grade Steel. The surfaces are ground and superfinished. The outside diameters are heavily crowned. The ends have a large machined radius designed to reduce friction between the roller and the retaining ring. The larger bearings use multiple rollers per pocket to minimize slippage.

Machined Brass Roller Riding Retainer

Retainers are manufactured from brass. The roller slots are accurately machined to provide smooth operation of the roller assembly. The rollers are retained by a steel band placed over the outside diameter of the retainer.

Precision Ground Inner and Plates

Plates are manufactured from Carburizing Bearing Grade Steel. The surfaces are precision ground and superfinished.

Precision Ground Inner and Outer Compression Sleeves

Compression Sleeves are manufactured from various materials designed to provide controlled deflection. These components are match ground with the plates.

Custom Capabilities

Detailed Drawings are available on the listed Tandem Thrust bearing designs. Upon request for a specific part number, a drawing will be sent containing the information in the following drawing along with the rated dynamic capacity. Shaft and housing fits are also available upon request.

New designs can be engineered and produced in small volumes for example combination radial and thrust bearings, concave and convex designs, screw down thrust, etc.. Contact Application Engineering for assistance in developing a tandem bearing design that will satisfy your application requirements. Based on your design envelope, loads, speeds and desired life, our engineers will design a tandem thrust bearing for your application. Let our Application Engineering Staff help you.

Tandem Thrust Bearings ROLLWAY®

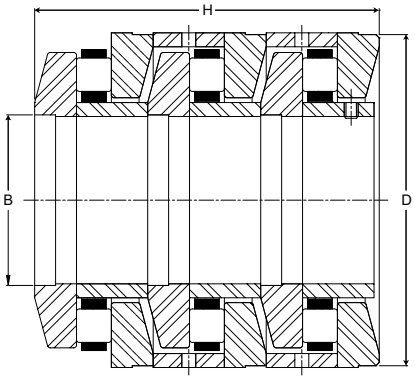
Basic Construction Type: Multi Stage Cylindrical Roller Thrust Bearing

Rolling Elements: Crowned Cylindrical Rollers

Bearing Material: Through Hardened Or Case Carburized Bearing Grade Steel

Series: 2, 3, 4, 6, Or 8 Stages

Retainer Types: Machined Brass



3 Stage

Part No.	B Bore inch mm	D O.D. inch mm	H Height inch mm	Basic Dynamic Rating lb N	Bearing Weight lb kg
TAC-014035-202	1.3775 34.989	3.5433 90.000	4.3750 111.125	93,600 419,330	7.9 3.6
TAC-022094-201	2.1654 55.001	9.4488 240.000	9.4488 240.000	66,700 298,820	113 51.3
TAC-030053-210	3.0000 76.200	5.3880 136.855	4.2500 107.950	155,000 694,400	10 4.5
TAC-030066-204	3.0000 76.200	6.6265 168.313	5.6000 142.240	160,800 720,380	33 14.9
TAC-040100-202	4.0000 101.600	10.0000 254.000	8.1250 206.375	458,000 2,051,840	120 54.4
TAC-101215-203	10.1000 256.540	21.5025 546.164	19.2500 488.950	2,572,000 11,522,560	1,050 476.2
TAC-120240-207	12.0000 304.800	24.0000 609.600	21.2500 539.750	3,460,000 15,500,800	1,800 816.5
TAC-170340-204	17.0000 431.800	34.0000 863.600	25.5200 648.208	5,220,000 23,385,600	3,399 1,541.7

Metric dimensions for reference only.
Not all parts are available from stock. Please contact customer service for availability (800) 626-2120.
For more information on bearing capabilities outside of our standard offering, please contact Application Engineering (800) 626-2093.

Thrust Bearing Engineering see page F-44.

For more information on bearing capabilities outside of our standard offering, please contact Application Engineering (800) 626-2093.

Load Ratings and Life

Life Calculations

The L10 (rating) life for any given application and bearing selection can be calculated in terms of millions of revolutions by using the bearing Basic Dynamic Rating and applied thrust load. The L10 life for any given application can be calculated in terms of hours, using the bearing Basic Dynamic Rating, applied load and suitable speed factors, by the following equation:

For thrust cylindrical roller and thrust tapered roller bearings:

$$L_{10} = \left(\frac{C}{P}\right)^{10/3} x \frac{1{,}000{,}000}{60 \times n} = \left(\frac{C}{P}\right)^{10/3} x \frac{16667}{n}$$

Where:

L_{10} = The # of hours that 90% of identical bearings under ideal conditions will operate at a specific speed and condition before fatigue is expected to occur.

C = Basic Dynamic Rating (lbs) 1,000,000 Revolutions

P = Constant Equivalent Load (lbs)

n = Speed (RPM)

Additionally, the ABMA provides application factors for all types of bearings which need to be considered to determine an adjusted Rated Life (Lna). L10 life rating is based on laboratory conditions yet other factors are encountered in actual bearing application that will reduce bearing life. Lna life rating takes into account reliability factors, material type, and operating conditions.

$$L_{na} = a_1 \times a_2 \times a_3 \times L_{10}$$

Where:

L_{na} = Adjusted Rated Life.

a_1 = Reliability Factor. Adjustment factor applied where estimated fatigue life is based on reliability other than 90% (See Table No 1).

a_2 = Material Factor. Life adjustment for bearing race material. Regal Power Transmission Solutions bearing races are manufactured from bearing quality steel. Therefore the a_2 factor is 1.0.

Table No. 1 Life Adjustment Factor for Reliability

Reliability %	L_{na}	a_1
90	L10	1
95	L5	0.62
96	L4	0.53
97	L3	0.44
98	L2	0.33
99	L1	0.21
50	L50	5

a_3 = Life Adjustment Factor for Operating Conditions. This factor should take into account the adequacy of lubricant, presence of foreign matter, conditions causing changes in material properties, and unusual loading or mounting conditions. Assuming a properly selected and mounted bearing having adequate seals and lubricant operating below 250°F and tight fitted to the shaft, the a3 factor should be 1.0.

Load Ratings and Life Continued

Vibration and shock loading can act as an additional loading to the steady expected applied load. When shock or vibration is present, an a3 Life Adjustment Factor can be applied. Shock loading has many variables which often are not easily determined. Typically, it is best to rely on one's experience with the particular application. Consult Application Engineering for assistance with applications involving shock or vibration loading.

The a3 factor takes into account a wide range of application and mounting conditions as well as bearing features and design. Accurate determination of this factor is normally achieved through testing and in-field experience. Regal Power Transmission Solutions offers a wide range of options which can maximize bearing performance. Consult Application Engineering for more information.

Variable Load Formula

Root mean load (RML) is to be used when a number of varying loads are applied to a bearing for varying time limits. Maximum loading still must be considered for bearing size selection.

$$RML^{*} = \sqrt[10/3]{\frac{(L_1^{10/3} N_1) + (L_2^{10/3} N_2) + (L_3^{10/3} N_3)}{100}}$$

Where:
RML = Root Mean Load (lbs.)
L_1, L_2, etc. = Load in pounds
N_1, N_2, etc. = Percent of total time operated at loads L_1, L_2, etc.

* Apply RML to rating at mean speed to determine resultant life.

Mean Speed Formula

The following formula is to be used when operating speed varies over time.

$$\text{Mean Speed} = \frac{S_1N_1 + S_2N_2 + S_3N_3}{100}$$

S_1S_2, etc = Speeds in RPM
N_1N_2, etc = Percentage of total time operated at speeds S_1S_2, etc

Load Ratings and Life Continued

Bearing Life In Oscillating Applications

The equivalent rotative speed (ERS) is used in life calculations when the bearing does not make complete revolutions during operation. The ERS is then used as the bearing operating speed in the calculation of the L10 (Rating) Life. The formula is based on sufficient angular rotation to have roller paths overlap.

ERS = Equivalent Rotative Speed

N = Total number of degrees per minute through which the bearing will rotate.

$$ERS = \frac{N}{360}$$

In the above formula, allowance is made for the total number of stress applications on the weakest race per unit time, which, in turn, determines fatigue life and the speed factors. The theory behind fretting corrosion is best explained by the fact that the rolling elements in small angles of oscillation retrace a path over an unchanging area of the inner or outer races where the lubricant is prevented by inertia from flowing in behind the roller as the bearing oscillates in one direction. Upon reversal, this small area of rolling contact is traversed by the same roller in the dry state. The friction of the two unlubricated surfaces causes fretting corrosion and produces failures which are unpredictable from a normal life standpoint.

With a given bearing selected for an oscillating application, the best lubrication means is a light mineral oil under positive flow conditions. With a light oil, there is a tendency for all areas in the bearing load zone to be immersed in lubricant at all times. The full flow lubrication dictates that any oxidized material which may form is immediately carried away by the lubricant, and since these oxides are abrasive, further wear tends to be avoided. If grease lubrication must be used, it is best to consult with either the bearing manufacturer or the lubricant manufacturer to determine the best possible type of lubricant. Greases have been compounded to resist the detrimental effect of fretting corrosion for such applications.

Static Load Rating

The “static load rating” for rolling element bearings is that uniformly distributed static radial load acting on a non-rotating bearing, which produces a contact stress of 580,000 psi (roller bearings) or 630,000 psi (ball bearings) at the center of the most heavily loaded rolling element. At this stress level, plastic deformation begins to be significant. Experience has shown that the plastic deformation at this stress level can be tolerated in most bearing applications without impairment of subsequent bearing operation. In certain applications where subsequent rotation of the bearing is slow and where smoothness and friction requirements are not too exacting, a higher static load limit can be tolerated. Where extreme smoothness is required or friction requirements are critical, a lower static load limit may be necessary.

Minimum Bearing Load

Skidding, or sliding, of the rolling elements on the raceway instead of a true rolling motion can cause excessive wear. Applications with high speeds and light loading are particularly prone to skidding. As a general guideline, rolling element bearings should be radially loaded at least 2% of Basic Dynamic Rating. For applications where load is light relative to the bearings dynamic load rating, consult Application Engineering for assistance.

Thrust Engineering Section

Rollway cylindrical roller thrust bearings are designed to support thrust loads (loads parallel to the axis of rotation) at relatively high speeds. Cylindrical roller thrust bearings are relatively stiff, require a minimum amount of axial space, and handle shock loading relatively well. Rollway manufactures four different styles of cylindrical roller thrust bearings:

1. Single Acting – Supports thrust or axial load in one direction.
2. Aligning – Accepts an initial static misalignment of nor more than 3 degrees.
3. Double Acting – Supports thrust or axial load in two directions.
4. Crane Hook Thrust – A shielded cylindrical roller thrust bearing that supports thrust or axial load in one direction.

Rollway tapered thrust bearings (TTHD and TTVF) are engineered for applications that contain high thrust loads and heavy shock loads. These bearings feature tapered or conical rollers positioned between two plates with tapered raceways. The tapered thrust bearing allows for true rolling motion with the vertex of the conical sections intersecting the bearing axis. The large end of each tapered roller is spherically ground. When the bearing is under load, this curvature guides the rollers accurately. The large spherical end of the roller is counterbored to improve lubrication between the roller and guide rib. By virtue of the additional contact surface, these bearings will have a higher dynamic rating than a similar sized cylindrical roller thrust bearing. Furthermore, they have superior performance in horizontal shaft applications. The self-centering action of the rollers counteract the gravitational effect of the roller assembly reducing the effects of the roller assembly contacting the shaft.

The tapered thrust bearings of the TTVF style are similar to the TTHD tapered thrust style except one thrust plate is flat. The guide rib on the one tapered raceway resists the induced radial force component caused by the inclined plane while the flat plate allows radial displacement without adversely affecting bearing operation. Maximum capacity is achieved through close spacing of the rollers through the use of a steel, hardened pin type retainer.

Rollway tandem thrust bearings, also referred to as multi-stage thrust bearings, were originally designed and patented by Rollway. The bearing consists of a series of thrust plates and roller assemblies with compression sleeves separating the stages. The design of the bearing sleeves and precision match grinding of the components allow the load to be equally applied through the stages of the bearing.

The tandem design allows the use of a high capacity bearing in a small area. Popular applications for this bearing type are rotary swivels, single screw extruders, and twin screw extruders. The tandem bearing allows for the increased output of machines without increasing the size of the gearbox. Rollway manufactures tandem bearings in two, three, four, six, and eight stages. Both inch and metric series sizes are available. Bore sizes range from about 1 to 22 inches with corresponding outside diameter ranging from 3.5 to 42 inches. Rollway tandem thrust bearings are supplied to original equipment manufacturers and the aftermarket.

Operating Conditions Factor

The life of a bearing is dependent on the operating conditions of the application. Lubrication, effects of the external environment, shaft and housing geometry and mounting, all have an effect on the actual bearing life. To determine a more realistic life calculation, the Operating Conditions Factor (F) can be included into the L_{10} life equation. The actual values determination will be based on experience of the designer and the expected operating conditions.

Using the Operating Conditions Factor (F) in the life equation, L_{10} life in hours now becomes:

$$L_{10} = F \times \left[\left(\frac{C}{P} \right)^{3.33} \times \frac{16667}{n} \right]$$

Thrust Engineering Section continued

Proper selection of the F factor demands intimate knowledge of the application. Where little is known of the application, it is recommended that F = 1 be selected. As a guide in selecting a realistic value for F, Rollway suggests use of the following, cumulative, individual sub-factors, f, to arrive at the over-all factor, F, thus:

$F = f_1 X f_2 X f_3 X f_4 .....$

The table below defines the application parameters and values recommended for derivation of the individual sub-factors.

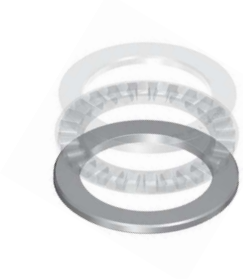
Thrust Bearing Factors

Factor	Application Condition	Factor Estimates	
		Poor	Excellent
f_1	Lubricant viscosity suitability @ bearing operating temperature (see Lubrication)	.5	1.0
f_2	External environment and provisions for isolation	.5	1.0
f_3	Operational conditions of shaft and housing squareness & rigidity	.5	1.0
f_4	Bearing thrust plate backing system full backing vs partial backing	.5	1.0

Cylindrical Roller Thrust Shaft Plate

The bore of the shaft plate is precision ground for a line to loose fit on in relation to the shaft outside diameter. The shaft plate outside diameter has a turned finish and is smaller than the housing plate's outside diameter. The plate is made from either through-hardened or carburizing grade steel with hardness to Rockwell (Rc) 58-63. Upon request we can manufacture these components from either CEVM or VIMVAR grades of material or M- 50 tool steel for high temperature applications.

All thrust plates are accurately ground for flatness and parallelism of the roller riding and backing surfaces. The roller contacting surfaces of the plates are superfinished to provide for long life. Locating diameters are ground to obtain an accurate fit on the shaft.

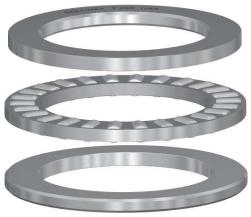


Cylindrical Roller Thrust Housing Plate

The outside diameter of the housing plate is precision ground for a line to loose fit in housing bore. The inside diameter has a turned finish and is larger than the shaft plate's inside diameter. The plate is made from either through-hardened or carburizing grade steel with hardness to Rockwell (Rc) 58-63. Upon request we can manufacture these components from either CEVM or VIMVAR grades of material or M- 50 tool steel for high temperature applications.

All thrust plates are accurately ground for flatness and parallelism of the roller riding and backing surfaces. The roller contacting surfaces of the plates are superfinished to provide for long life. Locating diameters are ground to obtain an accurate fit in the housing.

Thrust Engineering Section continued



Cylindrical Roller Thrust Roller Assembly

The roller assembly contains a machined brass roller-riding cage. Rollway thrust bearing retainers are machined from centrifugally cast brass. The retainers for all cylindrical roller thrust bearings are designed to be roller riding. The contoured roller pockets are accurately machined at right angles to the thrust force, which will be applied to the bearing. The rollers are retained in the assembly by a steel ring pinned to the outside diameter of the retainer.

The rollers in the roller assembly are matched to have outside diameters within .0001 inches. It should be noted that the Rollway design has a sphered roller end, which rides against the steel retaining ring for reduced wear. (The center of the contact point has zero velocity vs. the higher velocity that results from a flat ended roller contacting the ring.) The rollers used in cylindrical thrust roller bearings are also crowned. For the benefits of crowning please refer to page F-9.

Tapered Thrust Bearing Plates

The tapered thrust plates and rollers are made from carburizing grade steel surface hardened to HRc 58 minimum. Other material grades such as CEVM or VIMVAR are available upon request. All thrust plates are accurately ground for flatness and parallelism of the roller riding and backing surfaces. Locating plate diameters are surface ground to obtain an accurate fit on the shaft or in the housing. The tapered roller contacting surfaces are ground to ensure satisfactory bearing operating life.

Tapered Thrust Bearing Rollers

The tapered rolling elements are precision ground to provide an even load over the contact surfaces. The rollers are crowned for optimum stress patterns. The large end of the rollers are spherically ground providing controlled contact between the rollers and the guide rib.

Tapered Thrust Bearing Retainer

The tapered thrust bearing retainers are of two designs. The first design is a machined retainer from a single piece of centrifugally cast brass. The second design is a two-piece retainer made from hardened steel rings.

Tolerances

Rollway thrust bearings are produced to standard tolerances as listed in the following tables. Thrust bearings are available to increased accuracy upon request. Cylindrical roller thrust bearings contain rollers having a diameter variation of .0001 inches maximum per bearing.

Thrust Engineering Section continued

600 Series, Single Direction, Flat Seats

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	1.1870 30.1498	0.0000 0.0000	0.0005 0.0127	0.0000 0.0000	0.0060 0.1524
1.1870 30.1498	1.3750 34.9250	0.0000 0.0000	0.0006 0.0152	0.0000 0.0000	0.0060 0.1524
1.3750 34.9250	1.5620 39.6748	0.0000 0.0000	0.0007 0.0178	0.0000 0.0000	0.0060 0.1524
1.5620 39.6748	1.7500 44.4500	0.0000 0.0000	0.0008 0.0203	0.0000 0.0000	0.0060 0.1524
1.7500 44.4500	1.9370 49.1998	0.0000 0.0000	0.0009 0.0229	0.0000 0.0000	0.0060 0.1524
1.9370 49.1998	2.0000 50.8000	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0060 0.1524
2.0000 50.8000	2.1250 53.9750	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0080 0.2032
2.1250 53.9750	2.5000 63.5000	0.0000 0.0000	0.0011 0.0279	0.0000 0.0000	0.0080 0.2032
2.5000 63.5000	3.0000 76.2000	0.0000 0.0000	0.0012 0.0305	0.0000 0.0000	0.0080 0.2032
3.0000 76.2000	3.5000 88.9000	0.0000 0.0000	0.0013 0.0330	0.0000 0.0000	0.0100 0.2540

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	2.8750 73.0250	0.0005 0.0127	0.0000 0.0000
2.8750 73.0250	3.3750 85.7250	0.0007 0.0178	0.0000 0.0000
3.3750 85.7250	3.7500 95.2500	0.0009 0.0229	0.0000 0.0000
3.7500 95.2500	4.1250 104.7750	0.0011 0.0279	0.0000 0.0000
4.1250 104.7750	4.7180 119.8372	0.0013 0.0330	0.0000 0.0000
4.7180 119.8372	5.0000 127.0000	0.0015 0.0381	0.0000 0.0000

Thrust Engineering Section continued

600 Series, Single Direction, Aligning Seat With Aligning Washers

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	1.1870 30.1498	0.0000 0.0000	0.0005 0.0127	0.0000 0.0000	0.0060 0.1524
1.1870 30.1498	1.3750 34.9250	0.0000 0.0000	0.0006 0.0152	0.0000 0.0000	0.0060 0.1524
1.3750 34.9250	1.5620 39.6748	0.0000 0.0000	0.0007 0.0178	0.0000 0.0000	0.0060 0.1524
1.5620 39.6748	1.7500 44.4500	0.0000 0.0000	0.0008 0.0203	0.0000 0.0000	0.0060 0.1524
1.7500 44.4500	1.9370 49.1998	0.0000 0.0000	0.0009 0.0229	0.0000 0.0000	0.0060 0.1524
1.9370 49.1998	2.0000 50.8000	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0060 0.1524
2.0000 50.8000	2.1250 53.9750	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0080 0.2032
2.1250 53.9750	2.5000 63.5000	0.0000 0.0000	0.0011 0.0279	0.0000 0.0000	0.0080 0.2032
2.5000 63.5000	3.0000 76.2000	0.0000 0.0000	0.0012 0.0305	0.0000 0.0000	0.0080 0.2032
3.0000 76.2000	3.5000 88.9000	0.0000 0.0000	0.0013 0.0330	0.0000 0.0000	0.0100 0.2540

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	3.0000 76.2000	0.0007 0.0178	0.0000 0.0000
3.0000 76.2000	3.3750 85.7250	0.0009 0.0229	0.0000 0.0000
3.3750 85.7250	3.6250 92.0750	0.0011 0.0279	0.0000 0.0000
3.6250 92.0750	3.8750 98.4250	0.0013 0.0330	0.0000 0.0000
3.8750 98.4250	4.5312 115.0925	0.0015 0.0381	0.0000 0.0000
4.5312 115.0925	5.0000 127.0000	0.0017 0.0432	0.0000 0.0000

Thrust Engineering Section continued

700 Series, Single Direction, Flat Seats

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
2.0000 50.8000	3.0000 76.2000	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0080 0.2032
3.0000 76.2000	3.5000 88.9000	0.0000 0.0000	0.0012 0.0305	0.0000 0.0000	0.0100 0.2540
3.5000 88.9000	6.0000 152.4000	0.0000 0.0000	0.0015 0.0381	0.0000 0.0000	0.0100 0.2540
6.0000 152.4000	9.0000 228.6000	0.0000 0.0000	0.0015 0.0381	0.0000 0.0000	0.0150 0.3810
9.0000 228.6000	10.0000 254.0000	0.0000 0.0000	0.0018 0.0457	0.0000 0.0000	0.0150 0.3810
10.0000 254.0000	12.0000 304.8000	0.0000 0.0000	0.0018 0.0457	0.0000 0.0000	0.0200 0.5080
12.0000 304.8000	18.0000 457.2000	0.0000 0.0000	0.0020 0.0508	0.0000 0.0000	0.0200 0.5080
18.0000 457.2000	22.0000 558.8000	0.0000 0.0000	0.0025 0.0635	0.0000 0.0000	0.0250 0.6350
22.0000 558.8000	30.0000 762.0000	0.0000 0.0000	0.0030 0.0762	0.0000 0.0000	0.0250 0.6350

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
5.0000 127.0000	10.0000 254.0000	0.0015 0.0381	0.0000 0.0000
10.0000 254.0000	18.0000 457.2000	0.0020 0.0508	0.0000 0.0000
18.0000 457.2000	26.0000 660.4000	0.0025 0.0635	0.0000 0.0000
26.0000 660.4000	34.0000 863.6000	0.0030 0.0762	0.0000 0.0000
34.0000 863.6000	44.0000 1,117.6000	0.0040 0.1016	0.0000 0.0000

Thrust Engineering Section continued

700 Series, Single Direction, Aligning Seat With Aligning Washers

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
2.0000 50.8000	3.0000 76.2000	0.0000 0.0000	0.0010 0.0254	0.0000 0.0000	0.0100 0.2540
3.0000 76.2000	3.5000 88.9000	0.0000 0.0000	0.0012 0.0305	0.0000 0.0000	0.0150 0.3810
3.5000 88.9000	6.0000 152.4000	0.0000 0.0000	0.0015 0.0381	0.0000 0.0000	0.0150 0.3810
6.0000 152.4000	9.0000 228.6000	0.0000 0.0000	0.0015 0.0381	0.0000 0.0000	0.0200 0.5080
9.0000 228.6000	10.0000 254.0000	0.0000 0.0000	0.0018 0.0457	0.0000 0.0000	0.0200 0.5080
10.0000 254.0000	12.0000 304.8000	0.0000 0.0000	0.0018 0.0457	0.0000 0.0000	0.0250 0.6350
12.0000 304.8000	18.0000 457.2000	0.0000 0.0000	0.0020 0.0508	0.0000 0.0000	0.0250 0.6350
18.0000 457.2000	22.0000 558.8000	0.0000 0.0000	0.0025 0.0635	0.0000 0.0000	0.0300 0.7620

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
5.0000 127.0000	10.0000 254.0000	0.0019 0.0483	0.0000 0.0000
10.0000 254.0000	18.0000 457.2000	0.0021 0.0533	0.0000 0.0000
18.0000 457.2000	26.0000 660.4000	0.0023 0.0584	0.0000 0.0000
26.0000 660.4000	34.0000 863.6000	0.0025 0.0635	0.0000 0.0000
34.0000 863.6000	44.0000 1,117.6000	0.0030 0.0762	0.0000 0.0000

Thrust Engineering Section continued

Crane Hook

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	2.0156 51.1962	0.0100 0.2540	0.0000 0.0000	0.0000 0.0000	0.0080 0.2032
2.0156 51.1962	3.0156 76.5962	0.0100 0.2540	0.0020 0.0508	0.0000 0.0000	0.0100 0.2540
3.0156 76.5962	6.0156 152.7962	0.0150 0.3810	0.0020 0.0508	0.0000 0.0000	0.0150 0.3810
6.0156 152.7962	10.1560 257.9624	0.0150 0.3810	0.0050 0.1270	0.0000 0.0000	0.0200 0.5080

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
2.5000 63.5000	4.0000 101.6000	0.0050 0.1270	0.0050 0.1270
4.0000 101.6000	6.0000 152.4000	0.0060 0.1524	0.0060 0.1524
6.0000 152.4000	10.0000 254.0000	0.0100 0.2540	0.0100 0.2540
10.0000 254.0000	34.0000 863.6000	0.0120 0.3048	0.0120 0.3048

Thrust Engineering Section continued

Tapered Roller Thrust

Bore Diameter		Bore Tolerance		Height Tolerance	
over	incl	high (+)	low (-)	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	12.0000 304.8000	0.0010 0.0254	0.0000 0.0000	0.0150 0.3810	0.0150 0.3810
12.0000 304.8000	24.0000 609.6000	0.0020 0.0508	0.0000 0.0000	0.0150 0.3810	0.0150 0.3810
24.0000 609.6000	36.0000 914.4000	0.0030 0.0762	0.0000 0.0000	0.0150 0.3810	0.0150 0.3810
36.0000 914.4000	48.0000 1,219.2000	0.0040 0.1016	0.0000 0.0000	0.0150 0.3810	0.0150 0.3810

Outside Diameter		Outside Diameter Tolerance	
over	incl	high (+)	low (-)
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	12.0000 304.8000	0.0010 0.0254	0.0000 0.0000
12.0000 304.8000	24.0000 609.6000	0.0020 0.0508	0.0000 0.0000
24.0000 609.6000	36.0000 914.4000	0.0030 0.0762	0.0000 0.0000
36.0000 914.4000	48.0000 1,219.2000	0.0040 0.1016	0.0000 0.0000

Thrust Engineering Section continued

Thrust Bearing Mounting

Suitable tolerances for the shaft and housings of the 600 and 700 series thrust bearings and the tapered thrust bearings are listed in the following tables. These tolerances will provide satisfactory radial guidance for the cylindrical and/or tapered thrust bearings. For further information on bearing mounting and installation, refer to page F-56 of this catalog

Cylindrical Thrust
Thrust Bearing Mounting Practice – Shaft and Housing Fits

Bearing		Shaft Diameter Deviation	
Bore Diameter		from Bore Diameter (-)	
over	incl	high	low
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	1.1250 28.5750	0.0005 0.0127	0.0015 0.0381
1.1250 28.5750	1.3125 33.3375	0.0006 0.0152	0.0016 0.0406
1.3125 33.3375	1.5000 38.1000	0.0007 0.0178	0.0017 0.0432
1.5000 38.1000	1.6875 42.8625	0.0008 0.0203	0.0018 0.0457
1.6875 42.8625	1.8750 47.6250	0.0009 0.0229	0.0019 0.0483
1.8750 47.6250	2.1250 53.9750	0.0010 0.0254	0.0020 0.0508
2.1250 53.9750	2.5000 63.5000	0.0011 0.0279	0.0021 0.0533
2.5000 63.5000	3.0000 76.2000	0.0012 0.0305	0.0022 0.0559
3.0000 76.2000	3.5000 88.9000	0.0013 0.0330	0.0023 0.0584
3.5000 88.9000	7.0000 177.8000	0.0015 0.0381	0.0025 0.0635
7.0000 177.8000	9.0000 228.6000	0.0015 0.0381	0.0030 0.0762
9.0000 228.6000	12.0000 304.8000	0.0018 0.0457	0.0033 0.0838
12.0000 304.8000	15.0000 381.0000	0.0020 0.0508	0.0035 0.0889
15.0000 381.0000	19.0000 482.6000	0.0020 0.0508	0.0040 0.1016
19.0000 482.6000	23.0000 584.2000	0.0025 0.0635	0.0045 0.1143
23.0000 584.2000	30.0000 762.0000	0.0030 0.0762	0.0055 0.1397

Thrust Engineering Section continued

Cylindrical Thrust
Thrust Bearing Mounting Practice – Shaft and Housing Fits continued

Bearing		Housing Diameter Deviation	
Outside Diameter		from Outside Diameter (+)	
over	incl	high	low
inch mm	inch mm	inch mm	inch mm
2.0000 50.8000	2.3750 60.3250	0.0015 0.0381	0.0005 0.0127
2.3750 60.3250	3.2500 82.5500	0.0017 0.0432	0.0007 0.0178
3.2500 82.5500	3.6875 93.6625	0.0019 0.0483	0.0009 0.0229
3.6875 93.6625	4.0000 101.6000	0.0021 0.0533	0.0011 0.0279
4.0000 101.6000	4.5312 115.0925	0.0028 0.0711	0.0013 0.0330
4.5312 115.0925	10.0000 254.0000	0.0030 0.0762	0.0015 0.0381
10.0000 254.0000	18.0000 457.2000	0.0040 0.1016	0.0020 0.0508
18.0000 457.2000	22.0000 558.8000	0.0050 0.1270	0.0025 0.0635
22.0000 558.8000	26.0000 660.4000	0.0055 0.1397	0.0025 0.0635
26.0000 660.4000	28.0000 711.2000	0.0060 0.1524	0.0030 0.0762
28.0000 711.2000	34.0000 863.6000	0.0070 0.1778	0.0030 0.0762
34.0000 863.6000	38.0000 965.2000	0.0080 0.2032	0.0035 0.0889
38.0000 965.2000	44.0000 1,117.6000	0.0090 0.2286	0.0040 0.1016

Thrust Engineering Section continued

Tapered Thrust

Thrust Bearing Mounting Practice – Shaft and Housing Fits

Bearing		Spring Loaded Shaft Diameter Deviation	
Bore Diameter		from Bore Diameter (-)	
over	incl	high	low
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	6.8750 174.6250	0.0000 0.0000	0.0010 0.0254
6.8750 174.6250	7.9999 203.1975	0.0000 0.0000	0.0010 0.0254
7.9999 203.1975	12.0000 304.8000	0.0000 0.0000	0.0015 0.0381
12.0000 304.8000	24.0000 609.6000	0.0000 0.0000	0.0020 0.0508
24.0000 609.6000	36.0000 914.4000	0.0000 0.0000	0.0025 0.0635
36.0000 914.4000	48.0000 1,219.2000	0.0000 0.0000	0.0030 0.0762

Bearing		Housing Diameter Deviation	
Outside Diameter		from Outside Diameter (+)	
over	incl	high	low
inch mm	inch mm	inch mm	inch mm
0.0000 0.0000	10.5000 266.7000	0.0025 0.0635	0.0010 0.0254
10.5000 266.7000	13.0000 330.2000	0.0030 0.0762	0.0010 0.0254
13.0000 330.2000	20.0000 508.0000	0.0040 0.1016	0.0020 0.0508
20.0000 508.0000	25.0000 635.0000	0.0045 0.1143	0.0020 0.0508
25.0000 635.0000	30.0000 762.0000	0.0060 0.1524	0.0030 0.0762
30.0000 762.0000	35.0000 889.0000	0.0070 0.1778	0.0030 0.0762

Thrust Engineering Section continued

When mounting thrust bearings, there exists the possibility of a slight press fit due to the acceptable tolerances of the bearing bore and outside diameters. Under no circumstances should a press fit exceeding the limits shown be used with the thrust plates, as any expansion or contraction in the plates due to fit could result in a misalignment in the plates and subsequent limited bearing life.

Cylindrical and tapered roller thrust bearings require the support surfaces in the housing and the shaft to be at right angles to the shaft axis within .0005 inch per inch of diameter. For example, a four inch diameter shaft should be square to the shaft shoulder within .002 inches. The support surfaces should also provide for continuous support for the bearing thrust plates across the extent of the raceways. As a general rule, the minimum shaft shoulder and maximum housing shoulder should be as follows:

- Shaft shoulder at a minimum should be equal to the outside diameter of the shaft plate.
- Housing shoulder must have a maximum diameter to not exceed the inside diameter of the housing plate.

The tapered thrust bearing plates are manufactured with the same inside diameter and outside diameter on both plates. Applications using these bearings must be designed with ample clearance between the outside diameter of the shaft plate and the housing. Clearance must also be designed between the inside diameter of the housing plate and the shaft. It is recommended to provide for clearances of approximately .030 inches.

Tandem thrust bearings are designed to allow for the use of minimal shaft and housing shoulders. The cantilevering action of the thrust plates use of compression sleeves enable these bearings to be used effectively where only minimal shaft and housing shoulders exist.

Tandem Thrust Bearing Minimum Load

Tandem thrust bearings are designed to be used in horizontal shaft applications such as an extruder gear drive, and it is essential that a sufficient thrust load is applied to prevent roller skid. The minimum load required for tandem thrust bearings is expressed as a ratio of the bearing's dynamic rating (C) to the applied load (P). For ideal bearing operation, the C/P ratio should be less than 8. Bearing loads creating a C/P ratio greater than 12 must be avoided.

Lubrication

The required viscosity for the lubricant on cylindrical thrust bearings is 125 SSU at operating temperature. The required viscosity for the lubricant on tapered thrust bearings is 160 SSU at operating temperature. The required viscosity for the lubricant on tandem thrust bearings is 160 SSU at operating temperature. For further information in regards to thrust bearing lubrication please refer to page A-17 of this catalog.